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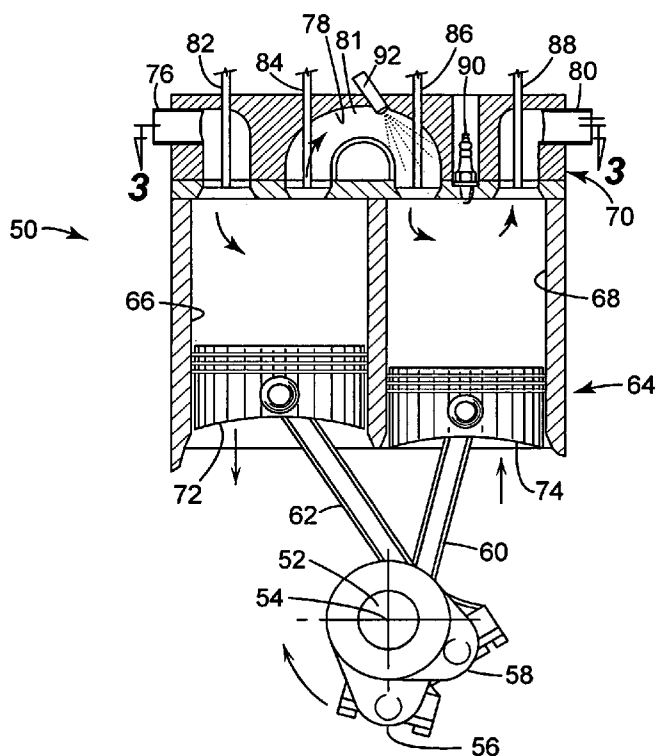
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(54) Title: SPARK PLUG LOCATION FOR SPLIT-CYCLE ENGINE

FIG. 2



(57) Abstract: A split-cycle engine includes separate compression and expansion cylinders connected by a crossover passage. Crossover compression and expansion valves define a pressure chamber between them in the crossover passage for storing pressurized gas prior to timed delivery into the expansion cylinder. One or more ignition sources, such as spark plugs, are positioned to encourage rapid combustion after ignition in the expansion cylinder but far enough from the crossover expansion valve(s) to prevent burning gases from reaching the crossover expansion valves before they are substantially closed to avoid entry of burning gas therein.

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**SPARK PLUG LOCATION FOR SPLIT-CYCLE ENGINE****CROSS REFERENCE TO RELATED APPLICATIONS**

This application claims the benefit of  
United States Provisional Patent Application No.  
5 60/963,742 filed August 7, 2007.

**TECHNICAL FIELD**

The present invention relates to internal  
10 combustion engines. More specifically, the present  
invention relates to location of an ignition source  
in an expansion cylinder of a split-cycle engine to  
avoid entry of burning air/fuel mixture into one or  
more crossover passage expansion valve ports prior to  
15 expansion valve closing timing.

**BACKGROUND OF THE INVENTION**

For purposes of clarity, the following  
20 definition is offered for the term "split-cycle  
engine" as may be applied to engines disclosed in the  
prior art and as referred to in the present  
application.

25 A split-cycle engine as referred to herein  
comprises:

a crankshaft rotatable about a crankshaft  
axis;

a compression piston slidably received within a compression cylinder and operatively connected to the crankshaft such that the compression piston reciprocates through an intake stroke and a  
5 compression stroke during a single rotation of the crankshaft;

an expansion (power) piston slidably received within an expansion cylinder and operatively connected to the crankshaft such that the expansion  
10 piston reciprocates through an expansion stroke and an exhaust stroke during a single rotation of the crankshaft; and

a crossover passage interconnecting the compression and expansion cylinders, the crossover  
15 passage including a crossover compression (XovrC) valve and a crossover expansion (XovrE) valve defining a pressure chamber therebetween.

United States Patent 6,543,225 granted  
20 April 8, 2003 to Carmelo J. Scuderi contains an extensive discussion of split-cycle and similar type engines. In addition, the patent discloses details of a prior version of an engine of which the present invention comprises a further development.

25

Referring to FIG. 1, an exemplary embodiment of the prior art split-cycle engine concept is shown generally by numeral 10. The split-cycle engine 10 replaces two adjacent cylinders of a  
30 conventional four-stroke engine with a combination of one compression cylinder 12 and one expansion cylinder 14. These two cylinders 12, 14 perform their respective functions once per crankshaft 16

revolution. The intake air and fuel charge is drawn into the compression cylinder 12 through typical poppet-style intake valves 18. The compression cylinder piston 20 pressurizes the charge and drives the charge through the crossover passage 22, which acts as the intake passage for the expansion cylinder 14.

A check type crossover compression (XovrC) valve 24 at the crossover passage inlet is used to prevent reverse flow from the crossover passage 22 into the compression cylinder 12. A crossover expansion (XovrE) valve 26 at the outlet of the crossover passage 22 controls flow of the pressurized intake charge such that the charge fully enters the expansion cylinder 14 shortly after the expansion piston 30 reaches its top dead center (TDC) position. Spark plug 28 is fired soon after the intake charge enters the expansion cylinder 14 and the resulting combustion drives the expansion cylinder piston 30 down toward bottom dead center (BDC). Exhaust gases are pumped out of the expansion cylinder through poppet exhaust valves 32.

With the split-cycle engine concept, the geometric engine parameters (i.e., bore, stroke, connecting rod length, compression ratio, etc.) of the compression and expansion cylinders are generally independent from one another. For example, the crank throws 34, 36 for each cylinder may have different radii and be phased apart from one another with top dead center (TDC) of the expansion cylinder piston 30 occurring prior to TDC of the compression cylinder

piston 20. This independence enables the split-cycle engine to potentially achieve higher efficiency levels and greater torques than typical four stroke engines.

5

Because the crossover expansion (XovrE) valve 26 has only a short time (about 30 degrees crank angle) to discharge pressurized air/fuel mixture into the expansion cylinder prior to completion of the compression cylinder piston stroke, closing of the crossover expansion valve occurs after ignition of the air/fuel charge. It is desired for extended valve life to avoid entry of burning fuel mixture into the crossover expansion valve without shortening the valve closing timing.

10  
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#### SUMMARY OF THE INVENTION

In a split-cycle engine according to the invention, the spark plug, or plugs, is (are) located in the expansion cylinder at a "safe distance" from the crossover expansion (XovrE) valve(s) wherein burning mixture from the ignition point will not reach the XovrE valve(s) before their substantial closing. This requires consideration in the design process of cylinder flame speed in the range of engine speeds as well as other considerations for location of the spark plug in conventional engines.

25

An engine according to the invention may include:

30

a crankshaft rotatable about a crankshaft axis of the engine;

a compression piston slidably received within a compression cylinder and operatively connected to the crankshaft such that the compression piston reciprocates through an intake stroke and a  
5 compression stroke during a single rotation of the crankshaft;

an expansion piston slidably received within an expansion cylinder and operatively connected to the crankshaft such that the expansion  
10 piston reciprocates through an expansion stroke and an exhaust stroke during a single rotation of the crankshaft;

a crossover passage interconnecting the compression and expansion cylinders, the crossover  
15 passage including a crossover compression (XovrC) valve and a crossover expansion (XovrE) valve defining a pressure chamber therebetween;

a cylinder head closing an end of the expansion cylinder and having a crossover expansion  
20 valve port seating the crossover expansion valve, and an ignition source having an ignition source center spaced from a nearest peripheral edge of the port of the crossover expansion valve and which ignites an  
25 air/fuel mixture at a prescribed ignition timing to establish a flame front of burning gases in the expansion cylinder;

wherein the ignition source center is positioned at a distance from the nearest peripheral  
30 edge of the crossover expansion valve port that is at least as great as a determined "safe distance" to avoid travel of burning gases into said crossover expansion valve port prior to substantial closing of said valve over at least a portion of engine

6

operating speeds, and the safe distance "S" is expressed by the function:

S (millimeters) = combustion speed  
(millimeters/crank angle degree) x crank angle  
5 degrees from ignition to crossover expansion valve  
closing.

Additional features may include:

10 The ignition source center is located  
sufficiently far from the cylinder wall to avoid  
cooling and quenching of the flame after ignition and  
not so far from cylinder walls as to overly extend  
burning time of the charge and cause self-ignition  
15 beyond the flame front.

The center of the ignition source is  
located at least 12mm from a nearest peripheral edge  
of an exhaust valve in the cylinder head to allow  
20 space for adequate cooling of the cylinder wall  
adjacent the ignition source.

These and other features and advantages of  
the invention will be more fully understood from the  
25 following detailed description of the invention taken  
together with the accompanying drawings.

#### **BRIEF DESCRIPTION OF THE DRAWINGS**

30 FIG. 1 is a transverse cross-sectional view  
of a prior art split-cycle engine related to the  
engine of the invention;



FIG. 2 is a transverse cross-sectional view of an exemplary split-cycle engine according to the present invention;

5 FIG. 3 is a cross-sectional top view of the split-cycle engine taken through line 3 - 3 of FIG. 2 with fuel injectors superimposed;

10 FIG. 4 is a bottom face view of the cylinder head showing key dimensions with relative locations of valves and ignition sources;

15 FIG. 5 is an illustration of flame penetration into a XovrE valve seat at 25 degrees ATDC, as the valve is closing;

20 FIG. 6 is a line graph of predicted "safe distance" between the ignition source center and the nearest peripheral edge of the XovrC valve port vs. engine speed; and

25 FIG. 7 is a two-dimensional diagram showing calculated flame progression at 1400 rpm from ignition at 14 degrees ATDC to 23 degrees ATDC.

#### **DETAILED DESCRIPTION OF THE INVENTION**

30 Referring now to FIGS. 2 and 3 of the drawings in detail, numeral 50 generally indicates a diagrammatic representation of a split-cycle engine according to the invention. Engine 50 includes a crankshaft 52 rotatable about a crankshaft axis 54 in a clockwise direction as shown in the drawing. The

crankshaft 54 includes adjacent angularly displaced leading and following crank throws 56, 58, connected to connecting rods 60, 62, respectively.

5 Engine 50 further includes a cylinder block 64 defining a pair of adjacent cylinders, in particular a compression cylinder 66 and an expansion cylinder 68 closed by a cylinder head 70 at one end of the cylinders opposite the crankshaft 52.

10

A compression piston 72 is received in compression cylinder 66 and is connected to the connecting rod 62 for reciprocation of the piston between top dead center (TDC) and bottom dead center  
15 (BDC) positions. An expansion piston 74 is received in expansion cylinder 68 and is connected to the connecting rod 60 for similar TDC/BDC reciprocation.

In an exemplary embodiment, the cylinder  
20 head 70 provides the means for gas flow into, out of and between the cylinders 66, 68. In the order of gas flow, the cylinder head includes an intake port 76 through which intake air is drawn into the compression cylinder 66, dual crossover (Xovr)  
25 passages 78 (at least one passage required), through which compressed air (gas) is transferred from the compression cylinder 66 to the expansion cylinder 68, and an exhaust port 80 through which spent gases are discharged from the expansion cylinder. Each  
30 crossover passage 78 also defines a pressure chamber 81 in which pressurized gas is stored when the crossover compression and expansion valves are closed.

Gas flow into the compression cylinder 66 is controlled by an inwardly opening poppet type intake valve 82. Gas flow into and out of each crossover passage 78 may be controlled by a pair of outwardly opening poppet valves, i.e. crossover compression (XovrC) valves 84 at inlet ends of the crossover passages and crossover expansion (XovrE) valves 86 at outlet ends of the crossover passages. Exhaust gas flow out the exhaust port 80 is controlled by an inwardly opening poppet type exhaust valve 88. These valves 82, 84, 86 and 88 may be actuated in any suitable manner such as by mechanically driven cams, variable valve actuation technology, or the like.

With continued reference to FIGS. 2 and 3 of the drawings, the exemplary engine 50 also includes one or more spark plugs 90 or other ignition sources located at appropriate locations in the end of the expansion cylinder wherein a mixed fuel and air charge may be ignited and burn during the expansion stroke.

Also the engine requires at least one fuel injector 92 operative to inject fuel into a charge of compressed air within at least one (or both) of the crossover passages 78 and pressure chambers 81.

With reference to FIG. 4, an embodiment of the spark ignition (SI) split-cycle engine 50 as shown has a cylinder head face 94 with dual crossover expansion (XovrE) valves 96 seated in XovrE valve

ports 98, wherein the XovrE valves open outwardly relative to the expansion cylinder 68 (not shown).

Cylinder head face 94 also includes at least one exhaust valve 100 seated in an exhaust valve port 102 and at least one ignition source 104, such as a spark plug, a glow plug, a switched laser or any controlled means of raising the fuel/air temperature sufficiently, at a location, to establish the start of combustion at that location. As discussed in greater detail herein, the center 106 of each ignition source 104 is located a safe distance "S" (designated with reference number 108) from a nearest peripheral edge 110 of each XovrE valve port 98. The relative positions of the XovrE valves 96, exhaust valve 100 and ignition sources 104 are important to:

- a) ensure good fuel mixing;
- b) promote appropriate charge motion in the cylinder;
- c) avoid flame burning into the crossover passage;
- d) avoid self-ignition ("detonation") of the fuel/air mixture before flame arrival. (Detonation is a phenomenon of uncontrolled self-ignition of pockets of unburned fuel and air which should generally be avoided in most spark-ignition engine operation); and
- e) achieve adequately fast burn before the piston descends too far.

There is an advantage to having twin ignition sources 104, in that the rate of burning is increased, and more importantly for the split-cycle engine 50, the use of twin ignition sources 104 provides more flexibility in realizing the minimum safe distance 108 from the nearest peripheral edge 110 of the XovrE valve port 98. This is because a single ignition source is usually placed at the center of the cylinder in order to provide equal flame path travel in all directions, thus providing relatively fast burn times compared to ignition sources that are offset. However, a central ignition source is not ideal for the split-cycle engine 50 as the center of a centrally located ignition source will tend to be closer to a nearest peripheral edge of the XovrE valve port 98 than the centers 106 of twin ignition sources 104 and will therefore be less likely to meet the minimum safe distance criterion versus twin ignition sources. Twin ignition sources 104 can be moved further from the cylinder center and the nearest peripheral edge of the XovrE valve port 98, while still achieving adequately fast burn times.

There are three main parameters which affect the selected location of the ignition sources 104 in the split-cycle engine 50:

Parameter 1. Distance to nearest peripheral edge 110 of XovrE valve ports 98

30

Referring to FIG. 5, in order to achieve combustion as close as possible to TDC in the split-cycle engine 50, it is necessary for ignition to

occur before the XovrE valves 96 have closed. However, it is also important to avoid flame 112 travel into the XovrE valve ports 98 for reasons of XovrE valve 96 durability and thermal efficiency losses. The centers 106 of the ignition sources 104 therefore need to be positioned sufficiently far from the nearest peripheral edge 110 of the XovrE valve ports 98 to allow the XovrE valves 96 to have substantially closed before the flame 112 reaches them. "Substantial" closure is taken to be at 23 degrees after top dead center (ATDC), as far as flame 112 penetration safety is concerned, though actual valve 96 closing is at 25 degrees ATDC. FIG. 5 shows that the flame 112 has reached, penetrated and overlapped the valve 96 at 23 degrees ATDC, but this is taken as acceptable as the valve/seat clearance is less than 0.5mm at 23 degrees ATDC when the flame arrives at the nearest peripheral edge 110 of the crossover expansion valve port 98.

20

Parameter 2. Distance to cylinder wall 68

Firstly, an ignition source 104 which is too close to the cylinder wall 68 (bore) can result in cooling and quenching of the flame 112, which is not ideal for promoting combustion in the early burning phase.

Secondly, an ignition source 104 which is too distant from any of the cylinder walls 68 will result in an extended burning time for the flame 112 to reach unburned mixture. This impairs thermal efficiency, and can result in self-ignition

30

(detonation) of the unburned mixture, due to compression of the unburned mixture and radiant heat transfer from the flame prior to flame arrival at the unburned mixture location.

5

For the first reason, the first and second ignition sources 104 are also typically at least 20% of the cylinder bore diameter from the periphery of the cylinder bore 68. For the second reason, a single  
10 ignition source 104 should not be more than ~60% of the cylinder bore diameter from any part of the cylinder wall area at the top of the cylinder bore 68.

15 Parameter 3. Distance to nearest peripheral edge of exhaust valve port 102

Adequate cooling passages, not shown, are necessary in the cylinder head water jacket between  
20 the spark plug boss, not shown, and the exhaust port 102 opening. The minimum distance is usually governed by casting limitations such as the minimum cast wall thickness that is possible as well as the minimum sand core section that is feasible for  
25 forming the cooling jacket. This requirement generally needs a minimum of 12mm between the center 106 of the ignition source 104 and the nearest peripheral edge of the exhaust valve port 102.

30 Referring to FIG. 6, graph 114 is derived from combustion computational fluid dynamics (CFD) prediction results and illustrates the significance of parameter 1 to the split-cycle engine 50. Line

116 depicts the distance traveled by the flame 112 (vertical axis of graph 114), from start of ignition to the point of crossover expansion valve 96 closing, versus engine speed (horizontal axis of graph 114) at full load conditions. If the ignition source 104 distance 108 from the nearest peripheral edge 110 of the XovrE valve port 98 is greater than the value indicated by line 116, this arrangement avoids flame 112 penetration into the crossover expansion valve port 98 before the crossover expansion valve 96 closes and may be called the "Safe Distance (S)." If the distance is less than the value indicated by line 116, this arrangement will result in flame penetration into the crossover expansion valve port 98 before the crossover expansion valve 96 closes. Graph 114 also shows that the theoretically safe distance is ~19mm at 1400rpm, flame speed 2.14mm/deg. (point 118) and 35mm at 4000rpm, flame speed 5.74mm/deg. (point 120). Point 122 is the actual location of the ignition sources 104 as modeled in the CFD analysis which generated this graph 114. Point 122 represents a safe distance of 19.8mm to enable optimum ignition at 1500rpm for engine 50.

25           The gradient of line 116 is dependent on both the combustion speed (speed of flame 112 front) at each engine speed, and the time from start of ignition, which varies at full load from ~14-20 degrees ATDC, to closing of the crossover expansion valve 96 at 25 degrees ATDC. For conventional 2 and 4-stroke combustion, the main combustion speed increases linearly with increasing engine speed while the time available for combustion to progress and



complete reduces linearly with increasing engine speed, these two factors resulting in an approximately constant angular period for complete combustion across the engine speed range. For the split-cycle engine 50, based on the CFD combustion predictions, the combustion speed at 4000rpm is approximately 2.5 times higher than the combustion speed at 1400rpm in a single plane ~1 millimeter (mm) below the cylinder head face 94, defined in millimeters/crank angle degree, and so approximately 1.8 times greater distance is required between the ignition source 104 and the crossover expansion valve 96 at 4000rpm than the safe distance required at 1400rpm.

15

The discrepancy between the 1.8 times "safe distances," and the 2.5 times angular combustion speed at 4000rpm and 1400rpm is probably due to several factors, the most significant being the longer angular period (9 degrees crank angle) at 1400rpm from ignition (14 degrees ATDC) to the safe closing point of the XovrE valve 96 (23 degrees ATDC), versus the equivalent period of 6 degrees ATDC at 4000rpm, due to the retarded ignition timing of 17 degrees ATDC at 4000rpm, the latter having been an early best estimate of ignition timing to avoid flame penetration into the XovrE port 98. If it is physically impossible to achieve the required safe distances between ignition source center 106 and the nearest peripheral edge 110 of the crossover expansion valve port 98, then the ignition must be delayed further from its timing after TDC and this will impair engine thermal efficiency.

Referring to FIG. 7, the approximate flame path travel between the ignition source 104 and the nearest peripheral edge 110 of the crossover expansion valve port 98 is deduced at 1400rpm by scaling the CFD contours of combustion progression, the flame front being taken as the 2000 degree K contour. In the example of FIG. 7, which is for a single central ignition, the 17 degrees ATDC contour is approximated as a simple white ellipse 124, progressing to the 23 degrees ATDC contour 126 at which combustion just reaches the nearest peripheral edge of the crossover valve port before the crossover valve's closure at 25 degrees ATDC. In FIG. 7, the scaled distance is approximately 19mm and this corresponds to the safe distance at 1400rpm (point 118) in FIG. 6.

Referring to FIG. 6, the combustion speeds at 1400rpm in the XovrE valve 96 direction can be calculated from the distance traveled between the two positions on the two 2000 degree K flame fronts, divided by the time or angular increments between each flame front at 1400rpm. These coarsely averaged combustion speeds at 1400rpm are 18 meters/second (m/s), or 2.14mm/crank degree, while the corresponding values at 4000rpm are 138m/s, or 5.74mm/crank degree, both these latter numbers having been incremented by nominal 30% from the scaled values to correct for the use of a lean air/fuel ratio in the 4000rpm CFD calculations.

For split-cycle engine 50 combustion chamber arrangements for gasoline fuels (as per FIG. 1 and FIG. 3), according to Parameter 1, the safe distance should be greater than 35mm; a lesser  
5 distance than 35mm will imply thermal efficiency losses at 4000rpm. For lower speeds, the safe distance can be reduced, for example to ~19mm at 1400 and probably pro rata between 19 and 35 mm for intermediate speeds. For example, a design value for  
10 the distance between the ignition source center 106 location and the nearest peripheral edge 110 of XovrE valve port 98 of 19.8mm provides optimum ignition up to ~1500rpm (point 122 in FIG. 6).

15 For greater safe distances, which would enable optimum ignition timing up to ~4000rpm, the ignition sources 104 should be moved closer towards the exhaust valve 100 (as per Parameters 2 and 3) and the crossover expansion valves 96 moved further from  
20 the ignition sources 104. A compromise has to be made because of the limited cylinder bore 68 size and the size of the exhaust valves 100, and it should be remembered that very off centered ignition arrangements are harmful to fast burn and to  
25 detonation, in most cases. The benefit of "inadequate" safe distance, such as 19.8mm, is that better burn times will be maintained for part load conditions where much lower combustion speeds are expected as a natural consequence of throttled engine  
30 operation. However, for hybrid applications, more full load operation would be required and this would probably demand the safe distances shown in FIG. 6.

It can be said that, subject to further knowledge of combustion speeds for the split-cycle engine 50, the predicted 19-35mm safe distance between ignition source center 106 and the nearest peripheral edge 110 of the XovrE valve ports 98, for 5 1400-4000rpm full load operation, is an absolute number applicable to all cylinder bore sizes for split-cycle engines operating on gasoline fuels. The safe distances would change if fuels with higher 10 laminar combustion speeds are used, or if some means is found for increasing the burning velocities, e.g. increased turbulence. Similar safe distances could be calculated for diesel operation, pending availability of CFD predictions.

15

In summary, the safe distance "S" for any split-cycle engine can be generally specified by the following relationship:

20  $S \text{ (mm)} = \text{combustion speed (millimeter/crank angle degree (mm/CAD))} \times \text{crank angle degrees from ignition to XovrE valve closing}$

More easily, S can be scaled from CFD 25 results showing ~23 degrees ATDC flame contour distance traveled from the ignition source for the operational speed range of the engine at full load, and the highest safe value distance selected according to the expected duty cycle of the engine; 30 above this selected speed, ignition would be retarded to avoid burning into the XovrE valve port 98.

The above expression can also be expressed in an analogous equation with combustion speed in m/s and time for combustion in seconds, as calculated from the engine speed and crank angle.

5

According to Parameter 2, both centers 106 of ignition sources 104 should be ~20% of the bore diameter from the periphery of cylinder bore 68, and according to Parameter 3, both centers 106 of  
10 ignition sources 104 should be at least 12mm from the nearest peripheral edge of the exhaust valve port 102.

This arrangement provides a combustion  
15 system which avoids burning into the crossover expansion valve port 98 before the crossover expansion valve 96 closes, while also achieving an optimum tradeoff between burning of the full cylinder 68 contents and avoidance of detonation.

20

Although the invention has been described by  
reference to specific embodiments, it should be understood that numerous changes may be made within the spirit and scope of the inventive concepts  
25 described. Accordingly, it is intended that the invention not be limited to the described embodiments, but that it have the full scope defined by the language of the following claims.

**CLAIMS**

What is claimed is:

- 5           1.    An    internal    combustion    engine  
comprising:  
          a crankshaft rotatable about a crankshaft  
axis of the engine;  
          a compression piston slidably received  
10 within a compression cylinder and operatively  
connected to the crankshaft such that the compression  
piston reciprocates through an intake stroke and a  
compression stroke during a single rotation of the  
crankshaft;
- 15           an expansion piston slidably received  
within an expansion cylinder and operatively  
connected to the crankshaft such that the expansion  
piston reciprocates through an expansion stroke and  
an exhaust stroke during a single rotation of the  
20 crankshaft;
- a crossover passage interconnecting the  
compression and expansion cylinders, the crossover  
passage including a crossover compression (XovrC)  
valve and a crossover expansion (XovrE) valve  
25 defining a pressure chamber therebetween; and
- a cylinder head closing an end of the  
expansion cylinder and having a crossover expansion  
valve port seating the crossover expansion valve, and  
an ignition source having an ignition source center  
30 spaced from a nearest peripheral edge of the port of  
the crossover expansion valve which ignites an  
air/fuel mixture at a prescribed ignition timing to

establish a flame front of burning gases in the expansion cylinder;

wherein the ignition source center is positioned at a distance from the nearest peripheral edge of the crossover expansion valve port that is at least as great as a determined "safe distance" to avoid travel of burning gases into said crossover expansion valve port prior to substantial closing of said valve over at least a portion of engine operating speeds, and the safe distance "S" is expressed by the function:

$$S \text{ (millimeters)} = \text{combustion speed (millimeters/crank angle degree)} \times \text{crank angle degrees from ignition to crossover expansion valve closing.}$$

2. The engine of claim 1 wherein the safe distance S is generally 19 millimeters (mm) or more.

3. The engine of claim 2 wherein the safe distance S is generally in the range of 19mm to 35mm.

4. The engine of claim 1 wherein the safe distance at 4000rpm is generally at least 1.8 times the safe distance at 1400rpm.

5. The engine of claim 1 wherein the ignition timing is retarded from an optimum value at a given engine operating speed.

6. The engine of claim 1 wherein the ignition source center is located sufficiently far

from the cylinder wall to avoid cooling and quenching of the flame after ignition and not so far from the cylinder wall as to overly extend burning time of the charge and cause self-ignition beyond the flame front  
5 from compression and radiant heating of the unburned charge.

7. The engine of claim 6 wherein the ignition source center is located not farther than 60  
10 percent of the expansion cylinder diameter from any part of the expansion cylinder wall adjacent the expansion cylinder closed end.

8. The engine of claim 6 wherein the  
15 ignition source center is located at least 20 percent of the cylinder diameter from the expansion cylinder wall adjacent the expansion cylinder closed end.

9. The engine of claim 1 wherein the  
20 cylinder head includes an exhaust port seating an exhaust valve, and the center of the ignition source is located at least 12mm from the nearest peripheral edge of the exhaust port to allow space for adequate cooling of the expansion cylinder wall adjacent the  
25 ignition source.

10. The engine of claim 1 wherein the crossover compression and crossover expansion valve open outwardly away from the cylinders.

30

11. The engine of claim 1 including at least two ignition sources per expansion cylinder.



12. The engine of claim 1 wherein the ignition source is at least a pair of ignition sources that each have an ignition source center that is at least the safe distance S from the nearest peripheral edge of the crossover expansion valve port.

13. The engine of claim 1 including two ignition sources and two crossover expansion valve ports, each ignition source having an ignition source center that is at least the safe distance S from the nearest peripheral edges of the crossover expansion valve ports;

wherein the centers of the ignition sources are further away from the nearest peripheral edges of the crossover expansion valve ports than a distance from a center of a centrally located ignition source to a nearest peripheral edge of each crossover expansion valve port.

**FIG. 1**  
**Prior Art**

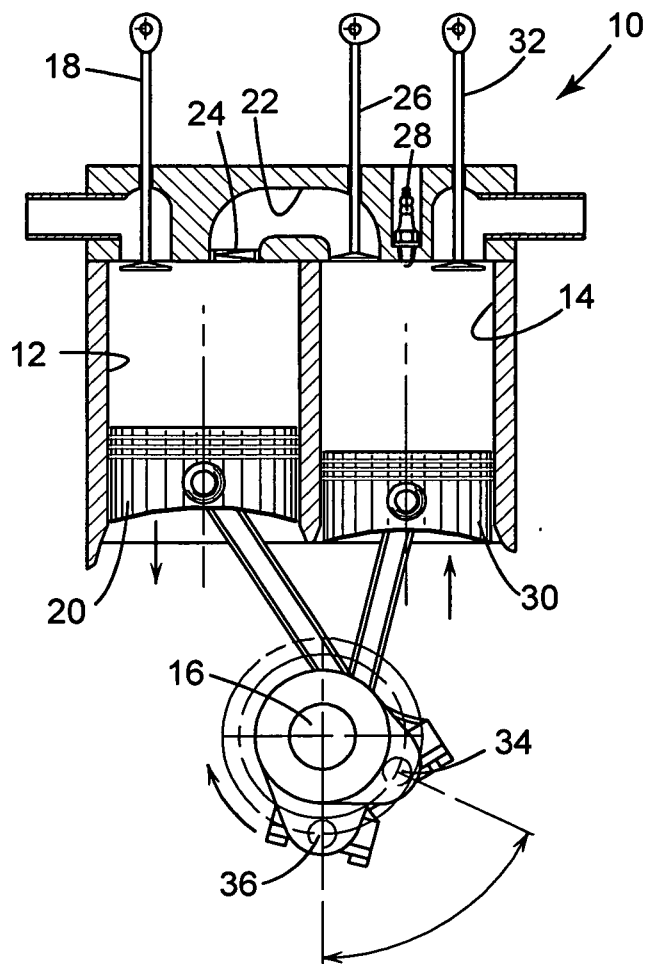


FIG. 2

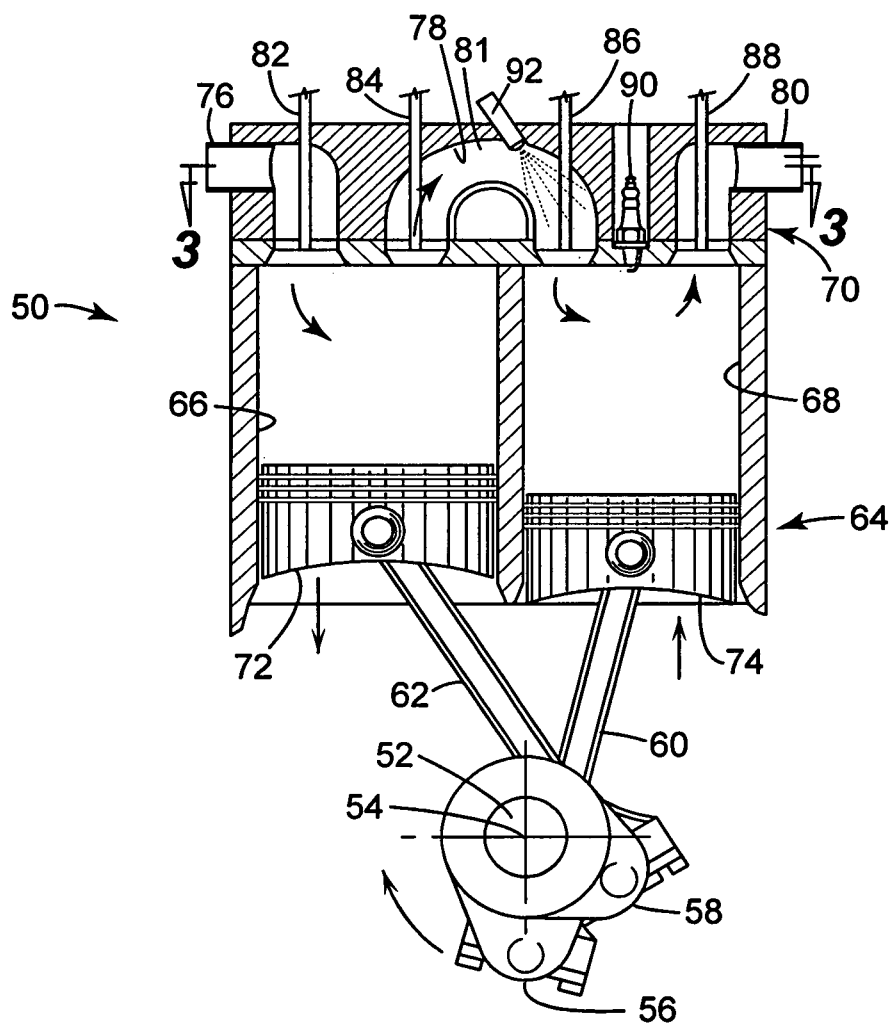
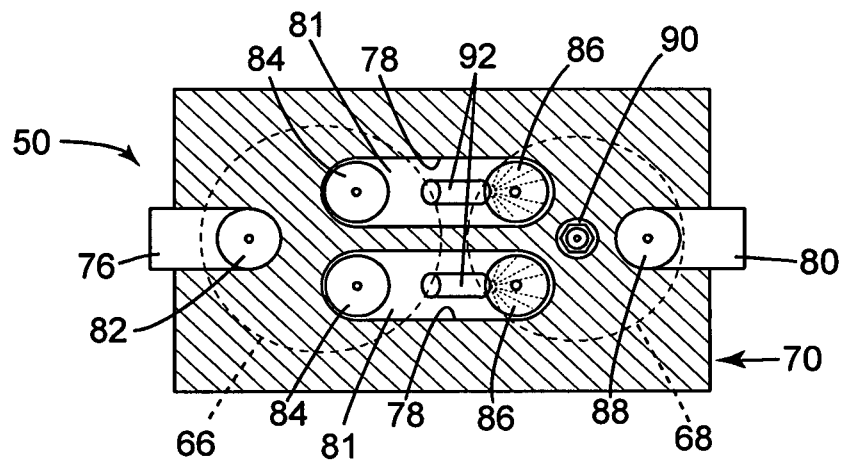
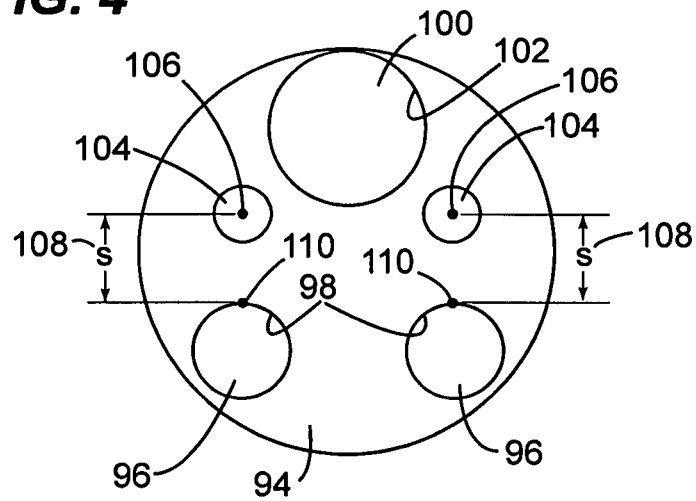


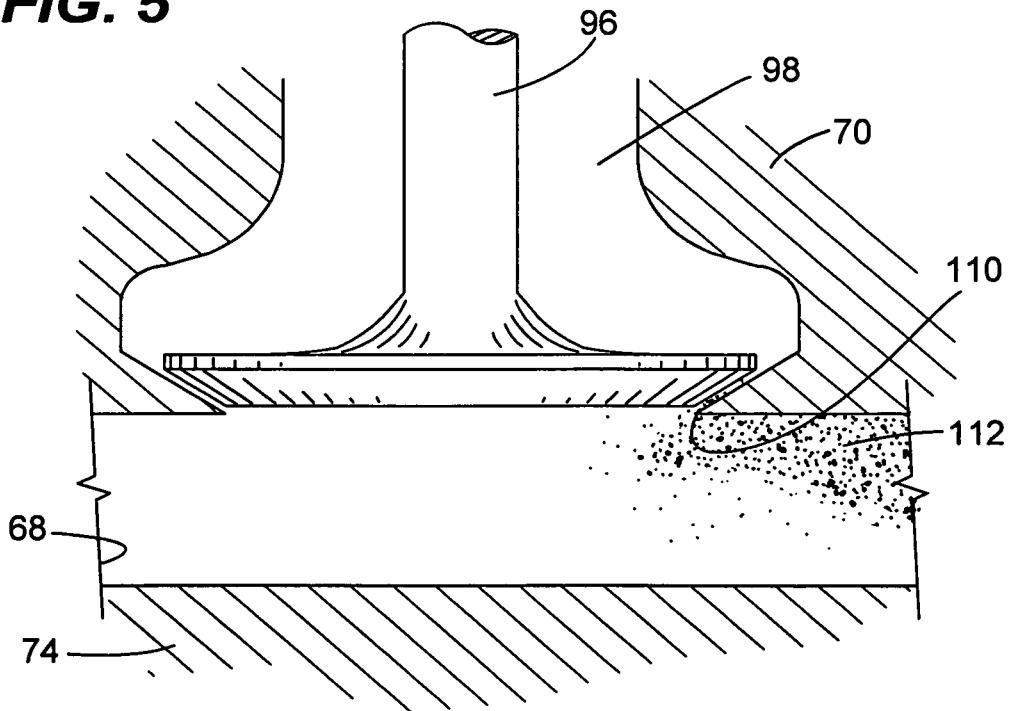
FIG. 3



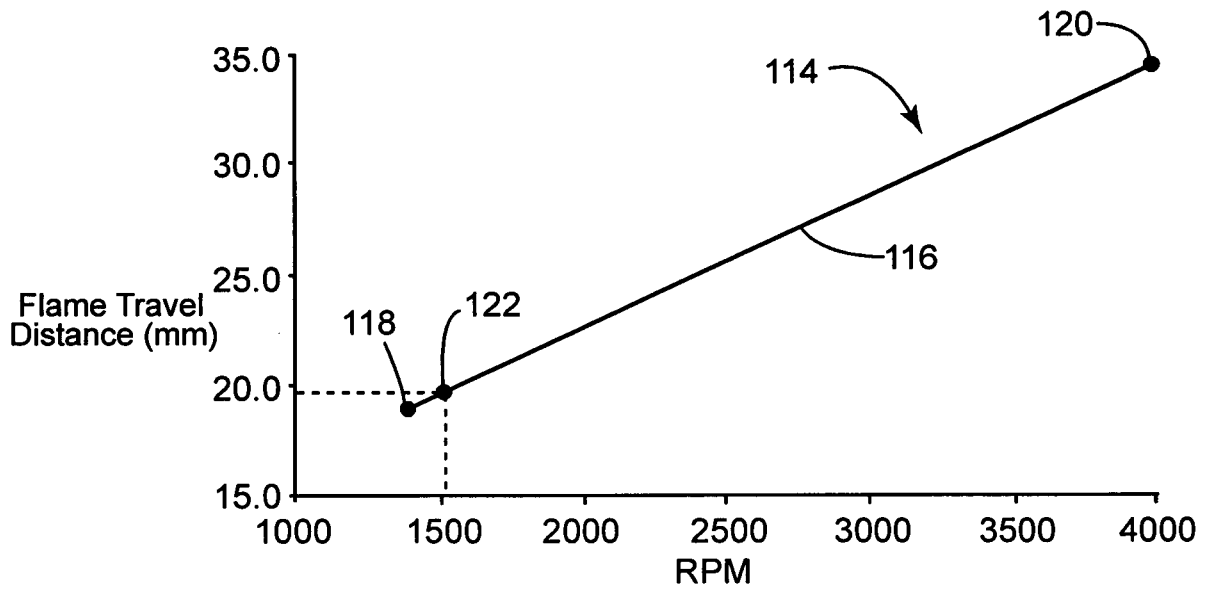
**FIG. 4**



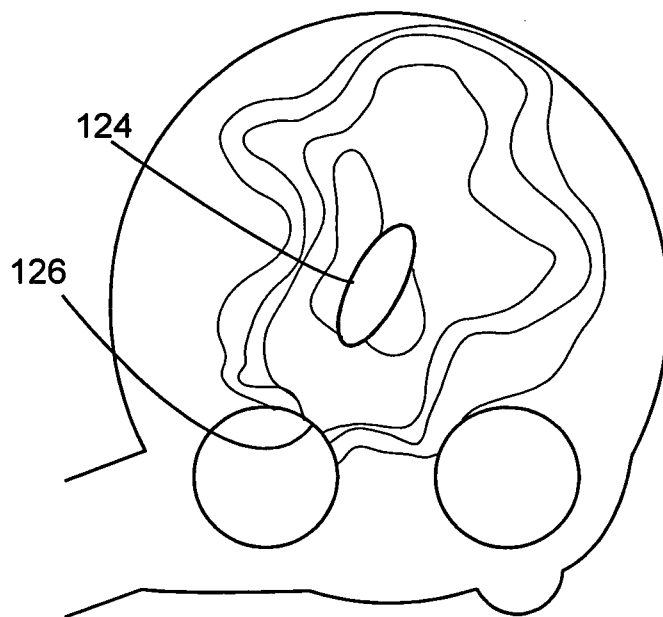
**FIG. 5**



**FIG. 6**



**FIG. 7**



## INTERNATIONAL SEARCH REPORT

International application No.

PCT/US 08/07312

## A. CLASSIFICATION OF SUBJECT MATTER

IPC(8) - F02B 25/00 (2008.04)

USPC - 123/70R

According to International Patent Classification (IPC) or to both national classification and IPC

## B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)

IPC(8) - F02B 25/00 (2008.04)

USPC - 123/70R

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  
USPC - 60/597, 620, 621, 622; 123/52.1, 53.1, 53.5, 58.8, 68, 70V (text search - see terms below)

Electronic data base consulted during the international search (name of data base and, where practicable, search terms used)

PubWEST(USPT,PGPB,EPAB,JPAB); Google Scholar; Google Patents

Search Terms: split, engine, crankshaft, compression, expansion, piston, cylinder, distance, ignition, plug, valve, combustion, retard, timing, open, outward, away, two, pair, multiple, cycle, combustion, multiple

## C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	US 6,543,225 B2 (Scuderi) 08 April 2003 (08.04.2003), Fig 7 and 9, col 5, ln 43-44, col 11, ln 57-59, col 12, ln 8-11	1-13
Y	US 6,494,178 B1 (Cleary et al.) 17 December 2002 (17.12.2002), Abstract and Claim 1	1-13
Y	US 4,186,561 A (Wishart) 05 February 1980 (05.02.1980), col 2, ln 28-32	5
Y	US 4,844,025 A (Sheaffer) 04 July 1989 (04.07.1989), Fig 1	11-13

 Further documents are listed in the continuation of Box C.

\* Special categories of cited documents:

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"&amp;" document member of the same patent family

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28 September 2008 (28.09.2008)

Date of mailing of the international search report

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